

Name _____

Please put answers within boxes provided.

Chemistry 342

October 23, 1998

Second Exam

Answers

$$1 \text{ J} = 1 \text{ kg m}^2 \text{ s}^{-2} \quad k_B = 1.38066 \times 10^{-23} \text{ J K}^{-1}$$

$$R = N_{\text{Avogadro}} k_B$$

$$R = 8.31441 \text{ J mol}^{-1} \text{ K}^{-1} = 1.98718 \text{ cal mol}^{-1} \text{ K}^{-1} = 0.082057 \text{ L atm mol}^{-1} \text{ K}^{-1}$$

$$C_p - C_v = \{ p + (\partial U / \partial V)_T \} (\partial V / \partial T)_p$$

$$(1/T) \{ -V + (\partial H / \partial p)_T \} = -(\partial V / \partial T)_p \quad (1/T) \{ p + (\partial U / \partial V)_T \} = (\partial p / \partial T)_V$$

$$\mu_{JT} = (\partial T / \partial p)_H \quad (\partial H / \partial p)_T = -C_p \mu_{JT}$$

$$\text{monatomic gas molar heat capacity: } C_v = (3/2)R$$

1. Consider the following cycle using 1 mole of an ideal gas, initially at 25°C and 1 atm pressure.

Step (1) Isothermal expansion against zero pressure to double the volume (Joule expansion).

Step (2) Isothermal, reversible compression from 1/2 atm to 1 atm.

(a) Calculate the value of $\oint dq/T$.

$n = 1 \text{ mol}$

For ideal gas $U = U(T)$ so that when T does not change $\Delta U = 0$. This holds for step 1 and step 2.

Step 1. $\Delta U = q + W$ First Law
 $0 = q_{\text{irrev}} + 0 \quad W = 0 \text{ since } P_{\text{op}} = 0$

Step 2. $\Delta U = q + W$
 $0 = q_{\text{rev}} - \int p dV \quad P_{\text{op}} = P_{\text{gas}} \text{ since reversible}$
or $dq_{\text{rev}} = +p dV = \frac{RTdV}{V} \text{ ideal gas}$

cycle:

$$\oint \frac{dq}{T} = \int_{\text{step 1}} \frac{dq_{\text{irrev}}}{T} + \int_{\text{step 2}} \frac{dq_{\text{rev}}}{T} = 0 + \int_{2V}^V \frac{RTdV}{TV} = R \ln \frac{1}{2}$$

$$= 8.3144 \text{ J mol}^{-1} \text{ K}^{-1} \times 1 \text{ mol} \times \ln \frac{1}{2} = -5.763 \text{ J K}^{-1}$$

(b) Calculate ΔS for Step (2)

$$\Delta S_2 = \int \frac{dq_{\text{REV}}}{T} = \text{as shown in part (a)} = R \ln \frac{1}{2} = -5.763 \text{ J K}^{-1}$$

(c) Calculate ΔS for Step (1)

$$\Delta S_1 = \int \frac{dq_{\text{REV}}}{T}$$

but since $\Delta S_{\text{cycle}} = 0$, $0 = \Delta S_1 + \Delta S_2$
 $0 = \Delta S_1 - 5.763 \text{ J K}^{-1}$
 $\therefore \Delta S_1 = +5.763 \text{ J K}^{-1}$

2. Given the following data for benzene, C_6H_6 :

At the normal boiling point, $80.1^\circ C$, $\Delta_{vap}H$ is $7.353 \text{ kcal mol}^{-1}$, and

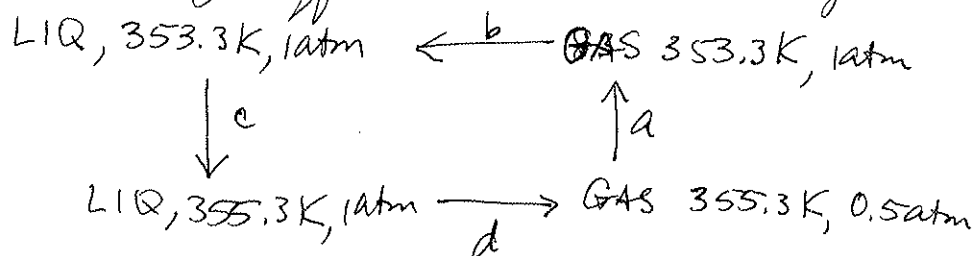
C_p for the liquid is $31 \text{ cal mol}^{-1} K^{-1}$

C_p for the vapor is $-0.409 + 77.621 \times 10^{-3} T - 264.29 \times 10^{-7} T^2 \text{ cal mol}^{-1} K^{-1}$

Assume that benzene vapor behaves ideally. Calculate ΔS for the process:

$C_6H_6 (\text{liq}, 82.1^\circ C, 1 \text{ atm}) \rightarrow C_6H_6 (\text{g}, 82.1^\circ C, 0.5 \text{ atm})$

This is not a reversible change since gas and liquid benzene are not at equilibrium at $82.1^\circ C$ as given. Therefore, we need to find ΔS by difference. Construct a cycle:



$$\Delta S_{\text{cycle}} = 0 = \Delta S_a + \Delta S_b + \Delta S_c + \Delta S_d \quad \text{Solve for } \Delta S_d$$

$$\int dS = \int \frac{C_p dT}{T} + \int \left(\frac{\partial S}{\partial p} \right)_T dp = \int \frac{C_p dT}{T} - \int \left(\frac{\partial V}{\partial T} \right)_p dp$$

problem 3(b) derivation

$$pV = RT \text{ ideal GAS}$$

$$V = RT/p$$

$$\left(\frac{\partial V}{\partial T} \right)_p = \frac{R}{p}$$

$$\Delta S = \int_{T_i}^{T_f} \frac{C_p dT}{T} - \int_{p_i}^{p_f} R \frac{dp}{p}$$

$$\Delta S_a = \int_{353.3}^{355.3} \frac{(-0.409 + 77.62 \times 10^{-3} T - 264.29 \times 10^{-7} T^2)}{T} dT - \int_{p_i=0.5}^{p_f=1 \text{ atm}} R \frac{dp}{p}$$

$$= -0.409 \ln \frac{355}{353} + 77.62 \times 10^{-3} (355 - 353) - 264.29 \times 10^{-7} \left(\frac{1}{2} \right) [353^2 - 355^2] - R \ln \left(\frac{1}{0.5} \right)$$

use $1.987 \text{ cal K}^{-1} \text{ mol}^{-1}$

continue 2. here $dS = dq_{rev}/T$

$$\Delta S_b = \frac{q_{rev}}{T} = \frac{-\Delta H_{vap}}{T_b} = \frac{-7.353 \times 10^3}{353.3} \text{ cal mol}^{-1} \text{ K}^{-1}$$

$$\Delta S_c = \int_{353}^{355} 31 \frac{dT}{T} + 0 = 31 \ln \frac{355}{353} \text{ cal mol}^{-1} \text{ K}^{-1}$$

$$0 = (31.409) \ln \frac{355}{353} + 77.62 \times 10^{-3} (-2) - 264.29 \times 10^{-7} \left(\frac{-1417.2}{2} \right) - 1.987 \ln 2$$

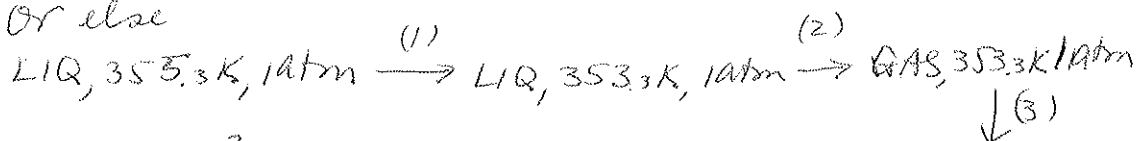
$$- \frac{7.353 \times 10^3}{353.3} + \Delta S_d = 0.1773 - 0.1552 + 0.01873 - 1.3773 + \Delta S_d$$

→ 20.812

$$0 = -22.15 + \Delta S_d$$

$$\therefore \Delta S_d = +22.15 \text{ cal mol}^{-1} \text{ K}^{-1}$$

Or else



$$\Delta S_1 = \int_{355}^{353} \frac{C_p^{LIQ}}{T} dT = 31.409 \ln \frac{353.3}{355.3} = -0.1773 \text{ cal mol}^{-1} \text{ K}^{-1}$$

$$\Delta S_2 = \frac{q_{rev}}{T} = \frac{\Delta_{vap} H}{T_b} = \frac{7.353 \times 10^3}{353.3} = +20.812 \text{ cal mol}^{-1} \text{ K}^{-1}$$

$$\Delta S_3 = \int_{353}^{355} \frac{C_p^{GAS}}{T} dT - \int_{1 \text{ atm}}^{0.5 \text{ atm}} \frac{R dp}{p} = +0.13647 + 1.3773 = +1.5138 \text{ cal mol}^{-1} \text{ K}^{-1}$$

$$\Delta S = \Delta S_1 + \Delta S_2 + \Delta S_3 = -0.1773 + 20.812 + 1.5138 = +22.15 \text{ cal mol}^{-1} \text{ K}^{-1}$$

3. (a) Derive $(\partial S / \partial p)_T$ for an ideal gas by making use of the First and Second Law and the fact that dG is an exact differential.

$$\begin{aligned}
 G &\equiv H - TS & H &= U + pV \\
 dG &= dU + p dV + V dp - T dS - S dT \\
 \text{First Law: } dU &= dq + dW \text{ whether reversible or irreversible} \\
 \text{Consider a reversible change: } dU &= dq_{\text{REV}} + dW_{\text{REV}} \\
 \text{Definition: } dS &= dq_{\text{REV}} / T & dW_{\text{REV}} &= -p dV \quad \left. \vphantom{\begin{aligned} dS &= dq_{\text{REV}} / T \\ dW_{\text{REV}} &= -p dV \end{aligned}} \right\} \rightarrow dU = T dS - p dV \\
 \text{Substitute into } dG &\text{ to get} \\
 dG &= T dS - p dV + p dV + V dp - T dS - S dT = \underline{V dp - S dT} \\
 \text{Since } dG &\text{ is an exact differential, therefore the} \\
 &\text{cross derivatives are equal,} \\
 -\left(\frac{\partial S}{\partial p}\right)_T &= \left(\frac{\partial V}{\partial T}\right)_p \quad \text{IDEAL GAS } pV = RT \quad V = RT/p \\
 &\quad \left(\frac{\partial V}{\partial T}\right)_p = R/p \\
 \therefore \left(\frac{\partial S}{\partial p}\right)_T &= -R/p \text{ for an ideal gas}
 \end{aligned}$$

(b) One mole of liquid water (density = 1 g/mL) is allowed to expand into an evacuated flask of volume such that the final pressure is 0.3 atm. The bulb containing the liquid and the flask are thermostated so that a constant temperature of 100 °C is maintained. It is found that 11,000 cal of heat are absorbed when this process occurs. Calculate the values for ΔU , ΔH , ΔS , and ΔG . Assume vapor is ideal.

$$\begin{aligned}
 \Delta U & \quad \text{LIQ, 1 atm, 373.2 K} \rightarrow \text{GAS, 0.3 atm, 373.2 K} \\
 p_{\text{top}} &= 0 \quad \therefore W = 0 \quad q = 11000 \text{ cal (given)} \\
 \Delta U &= q + W = \underline{11000 \text{ cal} + 0}
 \end{aligned}$$

$$\Delta H \quad H \equiv U + pV$$

$$\Delta H = \Delta U + \Delta(pV) = 11000 \text{ cal} + (pV)_{\text{GAS}} - (pV)_{\text{LIQUID}}$$

neglect $(pV)_{\text{LIQUID}}$ gas assumed ideal: $pV = RT$

$$\Delta H = 11000 \text{ cal} + 1.987(373) = \underline{11740 \text{ cal}}$$

ΔS is not $11000/373$

Construct a cycle

$$\Delta S_{\text{cycle}} = 0 = \Delta S_a + \Delta S_b + \Delta S_c$$

ΔS_a = as derived in problem 2

$$= \int C_p \frac{dT}{T} - \int \left(\frac{\partial V}{\partial T} \right) dp = 0 - \int_{p_i}^{p_f} R \frac{dp}{p} = -1.987 \ln \left(\frac{1}{0.3} \right)$$

$$\Delta S_b = \frac{q_{\text{REV}}}{373.2}$$

get q_{REV} for LIQ, 1 atm, 373.2 K $\rightarrow$ GAS, 0.3 atm, 373.2 K

from $\Delta U^* = 11000 \text{ cal} + 0$

and $W_{\text{REV}} = 1 \text{ atm} (V_{\text{GAS}} - V_{\text{LIQ}}) \approx R(373.2)$
 neglect 740 cal

$$\Delta S_b = \frac{-11740 \text{ cal}}{373.2 \text{ K}}$$

$$0 = -1.987 \ln \frac{1}{0.3} - \frac{11740}{373} + \Delta S_c \quad \therefore \Delta S_c = 33.87 \text{ cal/K}$$

ΔS continue here

ΔG As derived in 3(a): $dG = Vdp - SdT$

$$\Delta G_{\text{cycle}} = 0 = \Delta G_a + \Delta G_b + \Delta G_c \quad dT=0 \text{ for all steps}$$

$$\Delta G_a = \int_{0.3 \text{ atm}}^{1.0} V dp = RT \int_{0.3}^{1.0} \frac{dp}{p} = RT \ln \frac{1}{0.3} = 1.987(373.2) \ln \frac{1}{0.3} = 892.8 \text{ cal mol}^{-1}$$

$\Delta G_b = 0$ at 373.2 K LIQ and GAS are at equilibrium

$$0 = 1.987(373.2) \ln \frac{1}{0.3} + 0 + \Delta G_c$$

$$\Delta G_c = -892.8 \text{ cal}$$

[Get same answer by $\Delta G = \Delta H - T\Delta S$ from

$$\Delta H = 11740 \text{ cal mol}^{-1}$$

$$\Delta S = 33.85 \text{ cal K}^{-1} \text{ mol}^{-1}$$

See pages 7a and 7b for a useful overview based on this problem

An example of multiple approaches to a given problem:

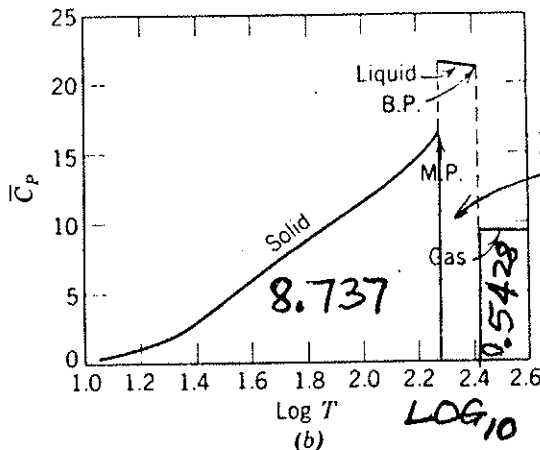
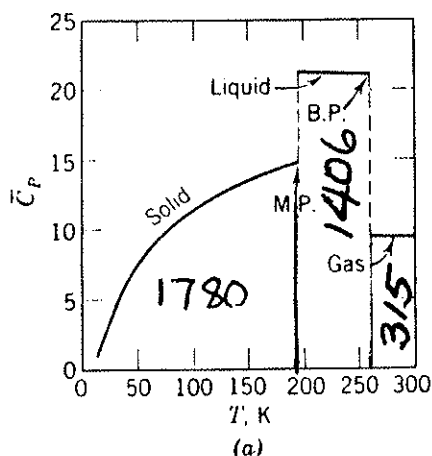
Exam Problem 3(b) One mole of liquid water (density = 1 g/mL) is allowed to expand into an evacuated flask of volume such that the final pressure is 0.3 atm. The bulb containing the liquid and the flask are thermostated so that a constant temperature of 100 °C is maintained. It is found that 11,000 cal of heat are absorbed when this process occurs. Calculate the values for ΔU , ΔH , ΔS , and ΔG . Assume vapor is ideal.

$dT = 0$ for this system

	cal mol ⁻¹	from definition of the function	from relations derived from First and Second Law
ΔU	11,000	$q_{IRREV} + W_{IRREV} = 11,000 + 0$ $q_{REV} + W_{REV} = 12,633 + -1633 = 11,000$	$T\Delta S - \int pdV = 12,633 - 1633 = 11,000$
$\Delta(pV)$	740	$p_f V_f - p_i V_i = RT - 1\text{atm} \times 0.018 \text{ L mol}^{-1} = 741.2 - 0.436 \approx 740$	
ΔH	11,740	$\Delta U + \Delta(pV) = 11,000 + 740 = 11,740$	$T\Delta S + \int Vdp = 12,633 - 843 = 11,740$
$T\Delta S$	12,633	$q_{REV} = 12,633$	
ΔG	-893	$\Delta H - T\Delta S = 11,740 - (12,633) = -893$	$-\int SdT + \int Vdp = 0 + (-893) = -893$
$\int Vdp$	-893		
$\int pdV$	1633	$-W_{REV}$	
ΔA		$\Delta U - T\Delta S = 11,000 - (12,633) = -1633$	$-\int pdV - \int SdT = -1633 + 0 = -1633$
ΔS_{sys}	33.87 cal mol ⁻¹ K ⁻¹	$q_{REV}/T = 12,633/373 = 33.87$ $= \Delta_{vap} H/T - \int Rdp/p$ $= 11740/373 - R \ln(0.3/1)$ $= 31.47 + 2.39 = 33.86$	
ΔS_{surr}	-29.49	$(q_{REV})_{surr}/T = -11,000/373 = -29.49$	

	cal mol ⁻¹	from considering a function of two variables
ΔU	11,000	$\Delta_{vap}U = 11,000$ for phase change + from $dU = (\partial U/\partial T)_V dT + (\partial U/\partial V)_T dV$ $= 0 + 0$ total = 11,000
$\Delta(pV)$	740	
ΔH	11,740	$\Delta_{vap}H = 11,740$ for phase change + from $dH = (\partial H/\partial T)_p dT + (\partial H/\partial p)_T dp$ $= 0 + 0$
$T\Delta S$	12,633	
ΔG	-893	$\Delta_{vap}G = 0$ for phase change + from $dG = (\partial G/\partial T)_p dT + (\partial G/\partial p)_T dp$ $= -SdT + Vdp$ $= 0 + (-893) = -893$
$\int Vdp$	-893	
$\int pdV$	1633	$-W_{REV}$ {Note that ΔA gives the maximum work done by the system}
ΔA		$dA = (\partial A/\partial T)_V dT + (\partial A/\partial V)_T dV$ $= -\int SdT - \int pdV$ $= 0 - 1633 = -1633$
ΔS_{sys}	33.87 cal mol ⁻¹ K ⁻¹	$\Delta_{vap}H/T = 11740/373$ + for the next rev step: $dS = (\partial S/\partial T)_p dT + (\partial S/\partial p)_T dp$ $= 0 - (\partial V/\partial T)_p dp$ $= 0 - R \ln(0.3/1)$ $= +2.39$ total = $31.47 + 2.39 = 33.86$
ΔS_{surr}	-29.49	

4. The heat capacity of sulfur dioxide at a constant pressure of 1 atm at different temperatures is shown below. At 15 K the heat capacity at constant pressure of $\text{SO}_2(\text{s})$ is $0.90 \text{ cal mol}^{-1} \text{ K}^{-1}$. Solid SO_2 melts at 197.64 K, $\Delta_{\text{fus}} H$ is $1769 \text{ cal mol}^{-1}$. At this pressure, liquid SO_2 vaporizes at 263.08 K and the $\Delta_{\text{vap}} H$ is $5960 \text{ cal mol}^{-1}$. The heat capacity of SO_2 gas between 300 K and 1500 K is $\{6.15 + 13.8 \times 10^{-3} T - 91.0 \times 10^{-7} T^2 + 2.06 \times 10^{-9} T^3\} \text{ cal mol}^{-1} \text{ K}^{-1}$. Calculate the molar entropy value for SO_2 gas at 298.1 K.



Areas underneath the curves from 15 K to 298.1 K are given.

Heat capacity in $\text{cal K}^{-1} \text{ mol}^{-1}$ of sulfur dioxide at a constant pressure of 1 atm at different temperatures.

For 1 mole of SO_2 at 1 atm

$$S_{298.1} = S_{0\text{K}} + \Delta S_{(0 \rightarrow 15\text{K})} + \Delta S_{(15\text{K} \rightarrow 197.64\text{K})} + \Delta S_{197.64\text{K}}^{\text{fus}} + \Delta S_{(197.64 \rightarrow 263.08\text{K})} + \Delta S_{263.08\text{K}}^{\text{vap}} + \Delta S_{(263.08 \rightarrow 298.1\text{K})}$$

$S_{0\text{K}} = 0$ Third Law

$$\Delta S_{(0 \rightarrow 15\text{K})} = \int_0^{15} \frac{C_p}{T} dT = \int_0^{15} \frac{aT^3}{T} dT = \int_0^{15} aT^2 dT = \left. \frac{aT^3}{3} \right|_0^{15} = \frac{a}{3} (15)^3$$

Let $C_p = aT^3$
(Debye T^3 -cubed Law)

$$\text{But } C_p(15\text{K}) = 0.90 = aT^3 = a(15)^3$$

$$\therefore \Delta S_{(0 \rightarrow 15)} = 0.30 \text{ cal K}^{-1} \text{ mol}^{-1}$$

$$\Delta S_{(15 \rightarrow 197.64)} = \int_{15}^{197.64} \frac{C_p}{T} dT = \int_{15}^{197.64} C_p d(\ln T) = 2.303 \int_{15}^{197.64} C_p d(\log_{10} T)$$

$$= 2.303 \times 8.737 \text{ cal K}^{-1} \text{ mol}^{-1}$$

$$= 20.12 \text{ cal K}^{-1} \text{ mol}^{-1}$$

Area under the C_p curve in C_p vs $\log_{10} T$

4. continue here

$$\Delta S_{\text{fus}} = \frac{\Delta H_{\text{fus}}}{197.64} = \frac{1769}{197.64} = 8.95 \text{ cal K}^{-1} \text{ mol}^{-1}$$

$$\Delta S_{(197 \rightarrow 263.08)} = 2.303 \times \underbrace{2.588}_{\text{area under the } C_p \text{ curve}} = 5.96 \text{ cal K}^{-1} \text{ mol}^{-1}$$

$$\Delta S_{\text{vap}} = \frac{\Delta H_{\text{vap}}}{263.08} = \frac{5960}{263.08} = 22.65 \text{ cal K}^{-1} \text{ mol}^{-1}$$

$$\Delta S_{(263.08 \rightarrow 298.1 \text{ K})} = 2.303 \times \underbrace{0.5428}_{\text{area under the } C_p \text{ curve}} = 1.25 \text{ cal K}^{-1} \text{ mol}^{-1}$$

$$\begin{aligned} S_{298.1 \text{ K}} &= 0.30 + 20.12 + 8.95 + 5.96 + 22.06 + 1.25 \\ &= \underline{59.64 \text{ cal K}^{-1} \text{ mol}^{-1}} \end{aligned}$$

5. Two moles of a gas whose equation of state is $pV = RT + ap$ where $a = 0.020 \text{ L mol}^{-1}$ at 300 K, 0.025 L mol^{-1} at 400 K, 0.030 L mol^{-1} at 500 K, undergoes isothermal compression at 300 K from 1 atm to 11 atm. Calculate ΔU , ΔG , ΔS , ΔA , and ΔH for the gas. First, derive the expressions that are appropriate for this **non-ideal** equation of state.

In this space, derive the expressions that are appropriate for this **non-ideal** equation of state, that you will need in the calculations of the changes in thermodynamic quantities.

Not an ideal gas, therefore we will start with the 2 equations (GENERAL) given on page 1 to derive $\left(\frac{\partial U}{\partial V}\right)_T$ and $\left(\frac{\partial H}{\partial p}\right)_T$:

$$\frac{1}{T} \left[-V + \left(\frac{\partial H}{\partial p}\right)_T \right] = -\left(\frac{\partial V}{\partial T}\right)_p \text{ given}$$

$$\text{or } \left(\frac{\partial H}{\partial p}\right)_T = V - T \left(\frac{\partial V}{\partial T}\right)_p$$

$$\therefore \left(\frac{\partial H}{\partial p}\right)_T = a - T \frac{da}{dT} \quad *$$

$$\frac{1}{T} \left[p + \left(\frac{\partial U}{\partial V}\right)_T \right] = \left(\frac{\partial p}{\partial T}\right)_V \text{ given}$$

$$\text{or } \left(\frac{\partial U}{\partial V}\right)_T = T \left(\frac{\partial p}{\partial T}\right)_V - p$$

$$\therefore \left(\frac{\partial U}{\partial V}\right)_T = \frac{RT^2}{(V-a)^2} \frac{da}{dT} \quad *$$

Given $pV = RT + ap$ where $a = a(T)$
 rearr. $V = \frac{RT}{p} + a$

$$\left(\frac{\partial V}{\partial T}\right)_p = \frac{R}{p} + \frac{da}{dT}$$

$$\begin{aligned} V - T \left(\frac{\partial V}{\partial T}\right)_p &= \left(\frac{RT}{p} + a\right) - T \left(\frac{R}{p} + \frac{da}{dT}\right) \\ &= a - T \frac{da}{dT} \end{aligned}$$

Start with $\beta = \frac{RT}{V-a}$

$$\left(\frac{\partial p}{\partial T}\right)_V = R \left[\frac{1}{V-a} + \frac{T \frac{da}{dT}}{(V-a)^2} \right]$$

$$= \frac{R}{V-a} + \frac{RT \frac{da}{dT}}{(V-a)^2}$$

$$T \left(\frac{\partial p}{\partial T}\right)_V - p = T \left(\frac{R}{V-a} + \frac{RT \frac{da}{dT}}{(V-a)^2} \right) - \frac{RT}{V-a}$$

$$T \left(\frac{\partial p}{\partial T}\right)_V - p = \frac{RT^2}{(V-a)^2} \frac{da}{dT}$$

As already derived in prob. 3a)

$$\left(\frac{\partial S}{\partial p}\right)_T = -\left(\frac{\partial V}{\partial T}\right)_p$$

$$\therefore \left(\frac{\partial S}{\partial p}\right)_T = - \left[\frac{R}{p} + \frac{da}{dT} \right] \quad *$$

$$\left(\frac{\partial V}{\partial T}\right)_p = \frac{R}{p} + \frac{da}{dT} \text{ done above}$$

continue here derivations, as needed

a changes linearly with T 0.005 in 100 K

$$\therefore a = 0.02 + 0.005 \times 10^{-2} (T - 300) \text{ L mol}^{-1}$$

$$\frac{da}{dT} = 0.005 \times 10^{-2} \text{ L mol}^{-1} \text{ K}^{-1}$$

$$\Delta U \quad dU = \left(\frac{\partial U}{\partial T} \right)_V dT + \left(\frac{\partial U}{\partial V} \right)_T dV. \text{ This problem has } dT = 0$$

$$\therefore \Delta U = \int \left(\frac{\partial U}{\partial V} \right)_T dV = RT^2 \frac{da}{dT} \int_{V_i}^{V_f} \frac{dV}{(V-a)^2} = RT^2 \frac{da}{dT} \left[\frac{-1}{V-a} \right]_{V_i}^{V_f}$$

$$= RT^2 \frac{da}{dT} \left[\frac{1}{V_i - a} - \frac{1}{V_f - a} \right] = T \frac{da}{dT} [p_i - p_f]$$

$$= (300 \text{ K}) (0.005 \times 10^{-2} \text{ L mol}^{-1} \text{ K}^{-1}) (1 - 11) \text{ atm} = -0.15 \text{ Latm mol}^{-1}$$

$$\Delta U = -0.30 \text{ Latm for 2 moles}$$

can convert this to J by

$$\times \frac{8.3144 \text{ J}}{0.082056 \text{ Latm}} \text{ to get } -30.4 \text{ J}$$

$$\Delta U = \underline{-30.4 \text{ J}}$$

ΔG

For 2 moles

or else $\Delta G = \Delta H - T\Delta S$ since T constant = same answer
get these from below

$$\Delta S \quad dS = \left(\frac{\partial S}{\partial T} \right)_P dT + \left(\frac{\partial S}{\partial P} \right)_T dP \quad \text{Here } dT = 0$$

For 2 moles

$$\Delta S = -0.3945 \text{ L atm K}^{-1} \text{ or } -39.975 \text{ J K}^{-1}$$

$$\Delta A \quad A \equiv U - TS \quad dT=0 \quad \therefore \Delta A = \underbrace{\Delta U}_{\text{get from above}} - T \underbrace{\Delta S}_{\text{get from above}}$$

$$\Delta A = -30.4 \text{ J} - 300 \text{ K} (-39.475 \text{ J K}^{-1}) = +11962.1 \text{ J}$$

or else,

$$dA = -pdV - SdT \quad dT=0$$

$$\therefore \Delta A = -\int_{V_i}^{V_f} pdV = -\int_{V_i}^{V_f} \frac{RT}{V-a} dV = -RT \ln \frac{V_f - a}{V_i - a} = -RT \ln \frac{P_i}{P_f}$$

$$= -8.3144(300) \ln \frac{1}{11} = +5981.1 \text{ J}$$

for 2 moles $\Delta A = +11962.2 \text{ J}$

$$\Delta H \quad dH = \left(\frac{\partial H}{\partial T}\right)_p dT + \left(\frac{\partial H}{\partial p}\right)_T dp. \quad \text{Since } dT=0 \text{ here,}$$

$$\Delta H = \int_{P_i}^{P_f} \left(\frac{\partial H}{\partial p}\right)_T dp \quad \text{derived earlier}$$

$$\Delta H = \left(a - T \frac{da}{dT} \right) \int_{P_i}^{P_f} dp$$

$$= \left[0.020 \frac{\text{L mol}^{-1}}{\text{K}} - 300 \text{ K} (0.005 \times 10^{-2} \text{ K}^{-2}) \right] (P_f - P_i) = 0.05 \text{ L atm mol}^{-1}$$

For 2 moles

$$\Delta H = 0.10 \text{ Latm or } 10.133 \text{ J}$$

or $\Delta H = \underbrace{\Delta U}_{\text{from previous calc.}} + \Delta(pV)$

$$\Delta(pV) = \Delta(RT + ap) = a(P_f - P_i) = 0.20 \text{ L atm mol}^{-1}$$

$$= -0.30 \frac{\text{Latm}}{\text{mol}} + 0.40 \frac{\text{Latm}}{\text{mol}} = +0.10 \text{ Latm or } 10.133 \text{ J}$$