

Problem Set 14

Part I

$$\begin{aligned} \textcircled{1} \quad E_{J+1} - E_J &= B_e (J+1)(J+2) - B_e J(J+1) \\ &\quad - \alpha_e (v + \frac{1}{2})(J+1)(J+2) \\ &\quad + \alpha_e (v + \frac{1}{2}) J(J+1) \\ &\quad - D_e (J+1)^2 (J+2)^2 \\ &\quad + D_e J^2 (J+1)^2 \end{aligned}$$

$$E_{J+1} - E_J = 2B_e (J+1) - 2\alpha_e (v + \frac{1}{2})(J+1) - 4D_e (J+1)^3$$

For rigid rotor

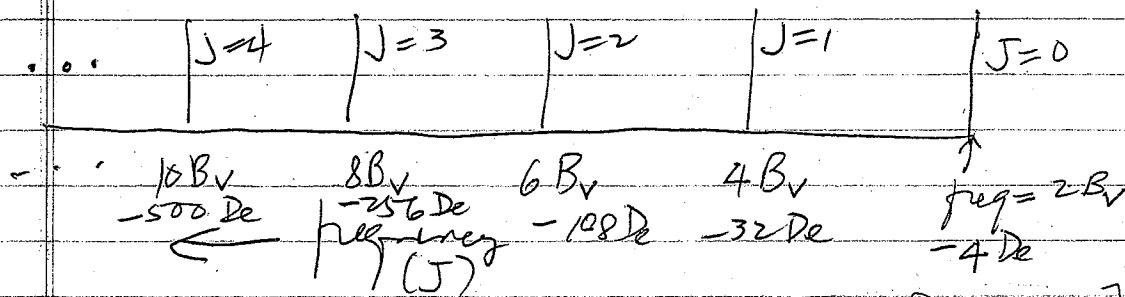
$$E_{J+1} - E_J = 2B_e (J+1)$$

deviation from rigid rotor increases with increasing J

microwave frequency:

$$\begin{aligned} \text{freq} &= 2B_e (J+1) - 2\alpha_e (v + \frac{1}{2})(J+1) - 4D_e (J+1)^3 \\ &= B_v 2(J+1) - 4D_e (J+1)^3 \end{aligned}$$

can almost neglect very small

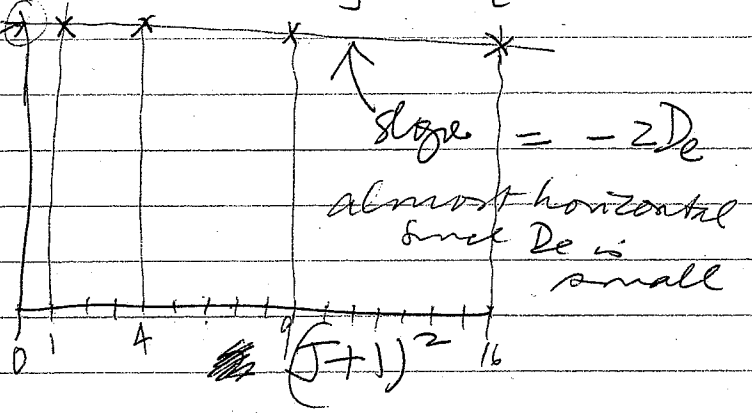


$$\begin{aligned} \text{frequency spacing} &= 2B_v - 4D_e [3J^2 + 9J + 7] \\ &= \text{freq}(J+1) - \text{freq}(J) \end{aligned}$$

$$f_{ug} = 2B_e(J+1) - 2\alpha_e(v+\frac{1}{2})(J+1) - 4D_e(J+1)^3 + \dots$$

$$\frac{f_{ug}}{2(J+1)} = [B_e - \alpha_e(v+\frac{1}{2})] - 2D_e(J+1)^2$$

Plot $\frac{f_{ug}}{2(J+1)}$



intercept = $B_v = B_e - \alpha_e(v+\frac{1}{2})$

slope = $-2D_e$

(2) for $\Delta J = +1$ $J_{upper} = J_{lower} + 1$

$$E_{v=1, J+1} - E_{v=0, J} = \frac{3}{2}v_e - x_e v_e (\frac{3}{2})^2 + y_e v_e (\frac{3}{2})^3 - \frac{1}{2}v_e + x_e v_e (\frac{1}{2})^2 - y_e v_e (\frac{1}{2})^3$$

$$+ B_e(J+1)(J+2) - B_e J(J+1) - D_e(J+1)^2(J+2)^2 + D_e J^2(J+1)^2 - \alpha_e \frac{3}{2} J(J+2) + \alpha_e \frac{1}{2} J(J+1)$$

actually can neglect D_e as too small

$$f_{ug} = v_e - 2x_e v_e + \dots \text{neglect } y_e v_e \text{ term}$$

$$\text{for } \Delta J = +1 \quad + 2B_e(J+1) - \alpha_e(J^2 + 4J - 3)$$

$$f_{ug} = v_e - 2x_e v_e + 2B_1(J+1) + (B_1 - B_0)J(J+1)$$

for $\Delta J = \pm 1$

$$R(J) = v_0 + 2B_1 + (B_1 - B_0)J + (B_1 - B_0)J^2$$

high frequency side
R branch

for $\Delta J = -1$ $J_{upper} = J_{lower} - 1$

$$E_{v=1, J-1} - E_{v=0, J} = \frac{3}{2} v_e - x_e v_e \left(\frac{3}{2}\right)^2 + y_e \left(\frac{3}{2}\right)^3 - \frac{1}{2} v_e + x_e v_e \left(\frac{1}{2}\right)^2 - y_e v_e \left(\frac{1}{2}\right)^3$$

$$+ B_e(J-1)(J) - x_e \frac{3}{2} (J-1)J - B_e J(J+1) + x_e \frac{1}{2} J(J+1)$$

neglecting D_e term as too small

low frequency side

for $\Delta J = -1$

$$freq = v_e - 2x_e v_e + \dots$$

neglecting y_e as too small also

$$- 2B_e J + x_e J(J-2)$$

except no $J_{lower} = 0$ term can occur

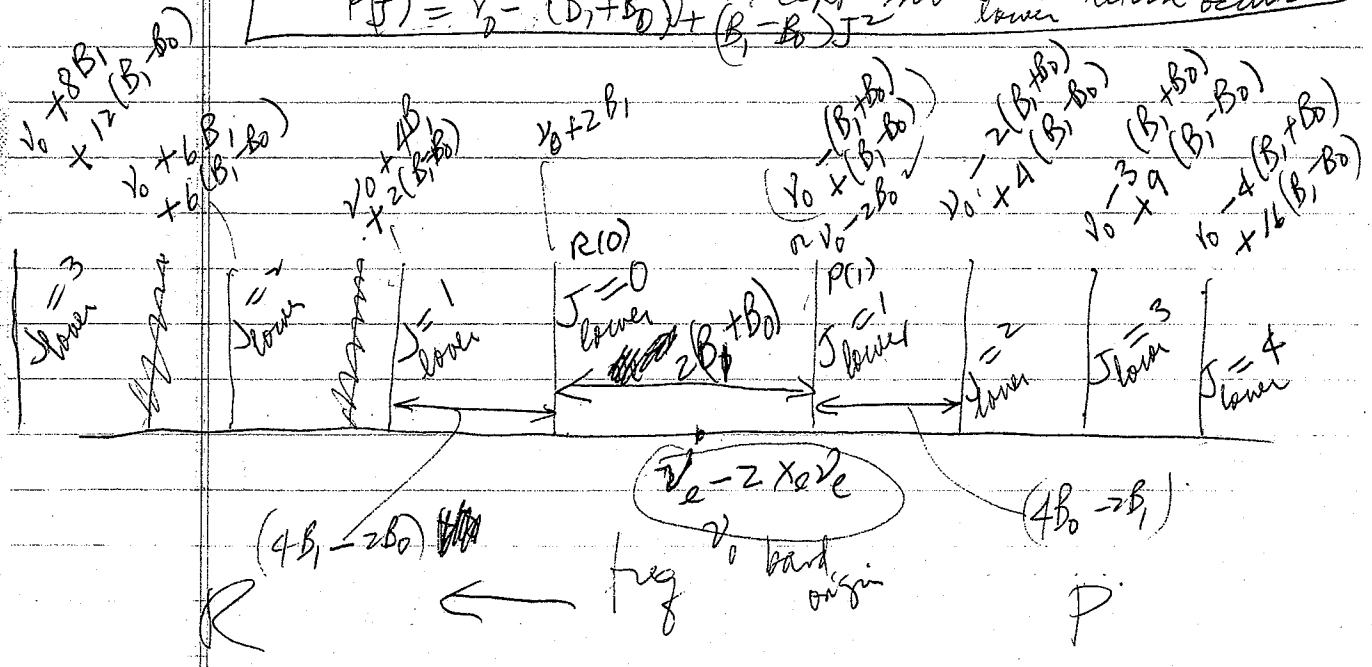
or

$$freq = v_e - 2x_e v_e + \dots + (B_1 - B_0) J^2 - (B_1 + B_0) J$$

for $\Delta J = -1$

$$P(J) = v_e - (B_1 + B_0) J + (B_1 - B_0) J^2$$

except no $J=0$ lower term can occur



low frequency side (P branch)

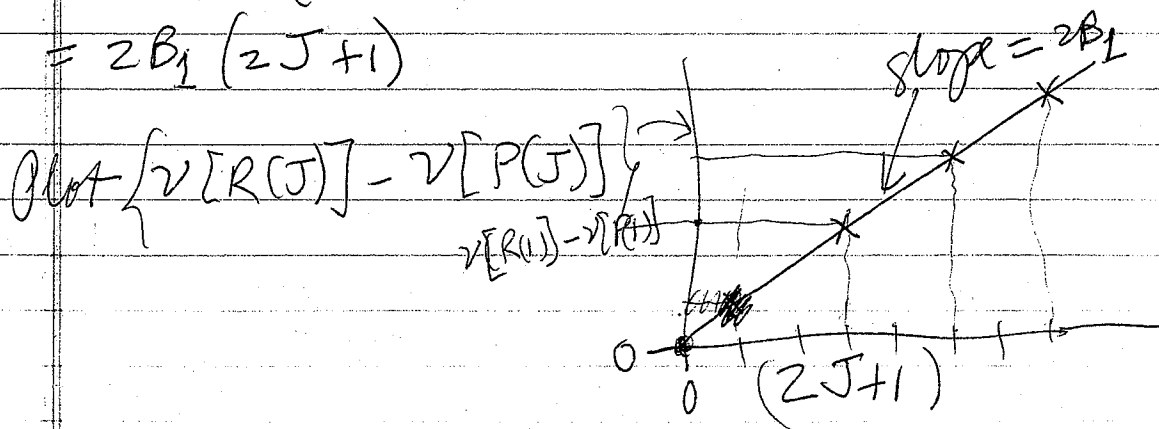
$$\begin{aligned} \text{spacing between two peaks} &= \nu[P(1)] - \nu[P(2)] \\ \text{closest to the band origin} &= \nu_0 - 2B_0 - [\nu_0 + 2B_1 - 6B_0] = 4B_0 - 2B_1 \end{aligned}$$

high frequency side (R branch)

$$\begin{aligned} \text{spacing between two peaks} &= \nu[R(1)] - \nu[R(0)] \\ \text{closest to the band origin} &= (\nu_0 + 6B_1 - 2B_0) - [\nu_0 + 2B_1] = 4B_1 - 2B_0 \end{aligned}$$

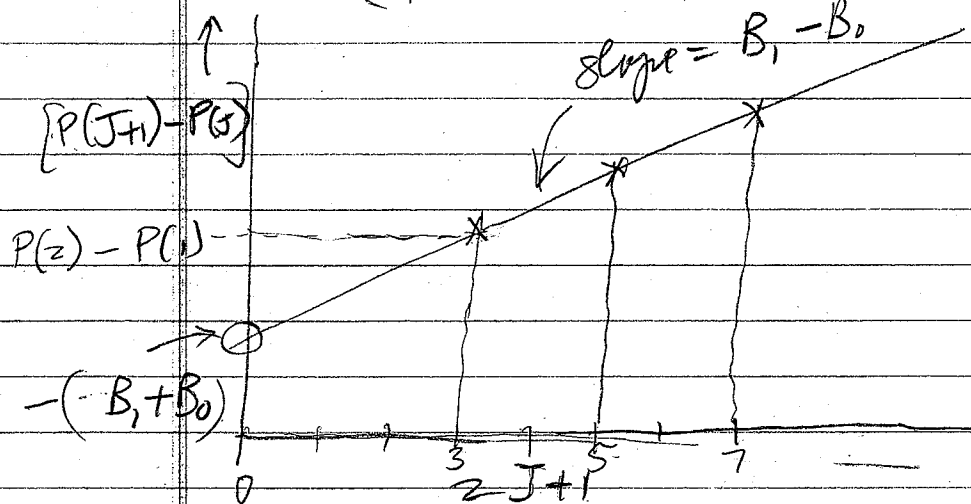
spacing between two peaks of same J_{lower}

$$\begin{aligned} &= \nu[R(J_{\text{lower}})] - \nu[P(J_{\text{lower}})] \\ &= \nu_0 + 2B_1 + (3B_1 - B_0)J + (B_1 - B_0)J^2 \\ &\quad - \{ \nu_0 - (B_1 + B_0)J + (B_1 - B_0)J^2 \} \\ &= 2B_1 + [(3B_1 - B_0) + (B_1 + B_0)]J = 2B_1 + 4B_1J \\ &= 2B_1(2J+1) \end{aligned}$$



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$$\begin{aligned}
 P(J+1) - P(J) &= v_0 - (B_1 + B_0)(J+1) + (B_1 - B_0)(J+1)^2 \\
 &\quad - [v_0 - (B_1 + B_0)J + (B_1 - B_0)J^2] \\
 &= -(B_1 + B_0) + (B_1 - B_0)(2J+1)
 \end{aligned}$$



$$\text{intercept} = -(B_1 + B_0)$$

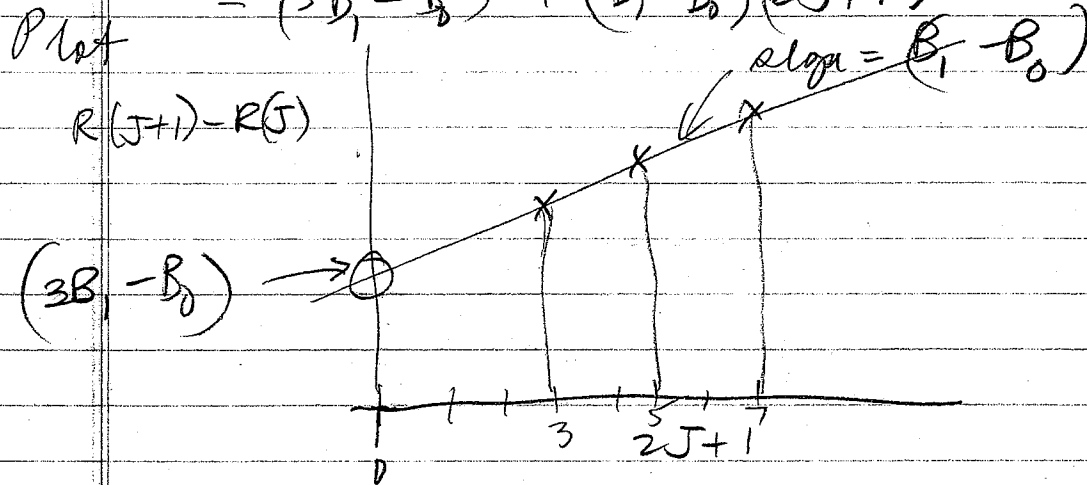
$$\text{slope} = B_1 - B_0$$

$$(\text{slope} - \text{intercept}) = 2B_1$$

$$(\text{intercept} + \text{slope}) = -2B_0$$

$$R(J+1) - R(J) = \cancel{v_0} + 2B_1 + (3B_1 - B_0)(J+1) + (B_1 - B_0)(J+1)^2 - [\cancel{v_0} + 2B_1 + (3B_1 - B_0)J + (B_1 - B_0)J^2]$$

$$= (3B_1 - B_0) + (B_1 - B_0)(2J+1)$$



$$\text{intercept} - \text{slope} = (3B_1 - B_0) - (B_1 - B_0)$$

$$= 2B_1$$

$$\text{intercept} - 3(\text{slope}) = (3B_1 - B_0) - 3(B_1 - B_0)$$

$$= 2B_0$$

To get $v_0 = v_c - 2x_c x_e$ after you have B_0 and B_1

$$P(1) = v_0 = 2B_0 \rightarrow v_0 = P(1) + 2B_0$$

$$R(0) = v_0 + 2B_1 \rightarrow v_0 = R(0) - 2B_1$$

③ $E_{v=0}^{① \text{ upper}} - E_{v''=0}^{② \text{ lower}} =$ neglect Δe and γ_e as too small 7

$$\underbrace{\{U_{\nu}(R_e') - U_{\nu}(R_e'')\}}_{T_e(\text{state})} + \frac{1}{2}(\nu_e' - \nu_e'') - \frac{1}{4}(\nu_e \nu_e' - \nu_e \nu_e'') \\ + B_0' J'(J'+1) - B_0'' J''(J''+1)$$

② For $J' = J'' + 1$ $\Delta J = +1$ lines

$$E_{v=0}' - E_{v''=0}'' = T_e + \frac{1}{2}(\nu_e' - \nu_e'') - \frac{1}{4}(\nu_e \nu_e' - \nu_e \nu_e'')$$

ν_0 band orig.

$P(J'')$

$$+ B_0' (J''+1)(J''+2) - B_0'' J''(J''+1)$$

$J''^2 + 3J'' + 2$

$J''^2 + J''$

$$\boxed{E_{v=0}' - E_{v''=0}'' = \nu_0 + 2B_0' + (3B_0' - B_0'')J'' + (B_0' - B_0'')J''^2}$$

high freq. side

⑥ For $J' = J'' - 1$ $\Delta J = -1$ lines

$$E_{v'=0}' - E_{v''=0}'' = \nu_0 + B_0' (J''-1)(J'') - B_0'' J''(J''+1)$$

$$\boxed{E_{v'=0}' - E_{v''=0}'' = \nu_0 - (B_0' + B_0'')J'' + (B_0' - B_0'')J''^2}$$

low freq. side

spacing between adjacent peaks in low freq. side:

$$P(J''+1) - P(J'') = \nu_0 - (B_0' + B_0'')(J''+1 - J'') + (B_0' - B_0'')[(J''+1)^2 - J''^2] \\ = \nu_0 - (B_0' + B_0'') + (B_0' - B_0'')(2J''+1)$$

$$\begin{aligned}
 \textcircled{c} \quad E'_{v'=1} - E''_{v''=0} &= [U_1'(R_e') - U_1''(R_e'')] + \frac{3}{2} \nu_e' - \frac{1}{2} \nu_e'' \\
 &\quad - \frac{9}{4} (x_e \nu_e') + \frac{1}{4} x_e \nu_e'' + B_1' J'(J'+1) - B_0'' J''(J''+1) \\
 &= \underbrace{\nu_{10}}_{\text{band origin}} + B_1' J'(J'+1) - B_0'' J''(J''+1) \\
 &\quad \text{standard for Te}(X) + \left(\frac{3}{2} \nu_e' - \frac{1}{2} \nu_e'' \right) - \frac{9}{4} x_e \nu_e' + \frac{1}{4} x_e \nu_e''
 \end{aligned}$$

① For $J' = J'' + 1$ or $\Delta J = +1$ lines

$$\begin{aligned}
 E'_{v'=1} - E''_{v''=0} &= \nu_{10} + B_1' (J''+1)(J''+2) - B_0'' J''(J''+1) \\
 R(J'') &= \nu_{10} + \underbrace{2B_1'}_{\text{high}} + \underbrace{(3B_1' - B_0'')}_{\text{high}} J'' + (B_1' - B_0'') J''^2
 \end{aligned}$$

② For $J' = J'' - 1$ or $\Delta J = -1$ lines

$$\begin{aligned}
 E'_{v'=1} - E''_{v''=0} &= \nu_{10} + B_1' (J''-1)J'' - B_0'' J''(J''+1) \\
 P(J'') &= \nu_{10} - (B_1' + B_0'') J'' + (B_1' - B_0'') J''^2 \\
 &\quad \text{low freq. side}
 \end{aligned}$$

spacing between adjacent peaks in low frequency side:

$$\begin{aligned}
 P(J''+1) - P(J'') &= -(B_1' + B_0'')(J''+1 - J'') + (B_1' - B_0'')[(J''+1)^2 - J''^2] \\
 &= -(B_1' + B_0'') + (B_1' - B_0'')(2J''+1)
 \end{aligned}$$

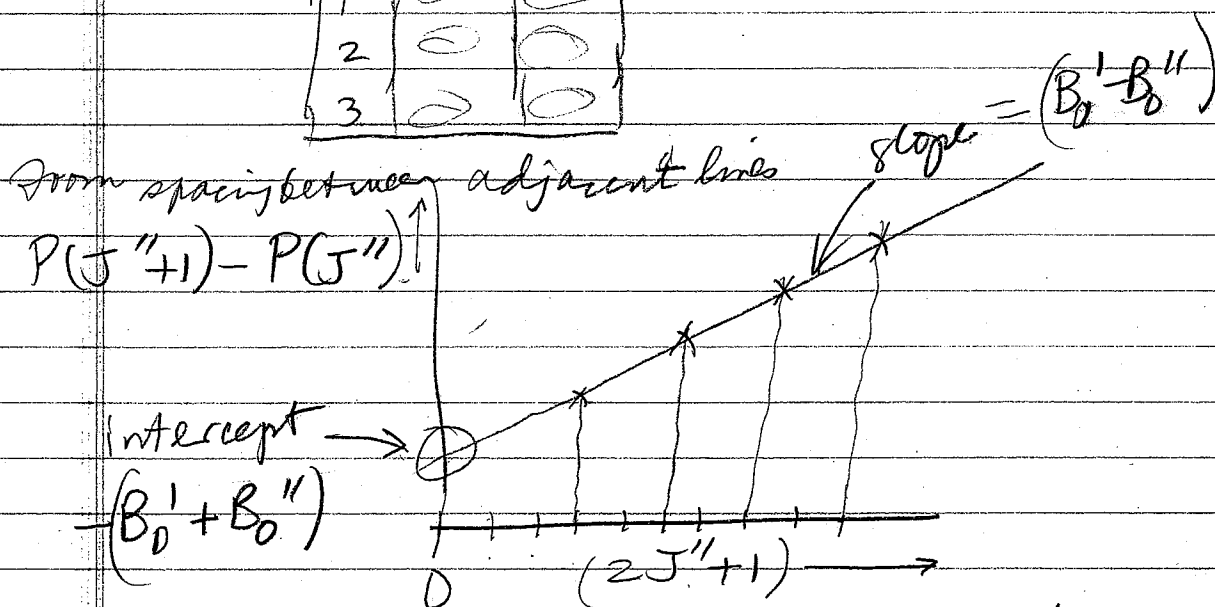
Given the $(E_{v'=0} - E_{v''=0})$ list of frequencies that is, the values $P(J'')$ and $R(J'')$

what can we make straight-line plots of data? $J'' = 1, 3, 5, \dots$ $J'' = 0, 1, 2, \dots$

frequencies

J''	$P(J'')$	$R(J'')$
0	—	○
1	○	○
2	○	○
3	○	○

give in all such numbers



$$b = -B_0' - B_0''$$

$$m - b = 2B_0' =$$

$$m = B_0' - B_0''$$

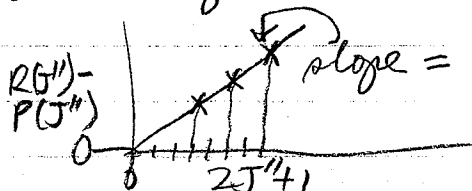
slope - intercept

$$b + m = -2B_0'' = \text{slope} + \text{intercept}$$

can get both B_0' and B_0'' from straight line plot

$$\text{From } R(J'') - P(J'') = 2B_0' + 2B_0'J'' = B_0'(2J''+1)$$

can get B_0'



From $P(1) = \nu_{00} - (B_0' + B_0'') + (B_0' - B_0'')^2$
 $= \nu_{00} - 2B_0''$

$$R(1) = \nu_{00} + 2B_0'$$

can get $\nu_{00} = T_e(\nu') + \frac{1}{2}(\nu' - \nu'') - \frac{1}{4}(x_e \nu' - x_e \nu'')$
 if we first get B_0' or B_0'' from previous plots.

(4) Rotational Raman, end up in same v , i.e. $v = v'' = 0$
 $E_{v'J'} = E_{v''J''} = B_0 [J'(J'+1) - J''(J''+1)]$

$\Delta J = +2$ $J' = J'' + 2$ S branch begins with $J''=0$

$$S(J'') = B_0 \left[\underset{J^2 + 5J + 6}{(J''+2)(J''+3)} - \underset{J^2}{J''(J''+1)} \right]$$

$$= B_0(4J'' + 6)$$

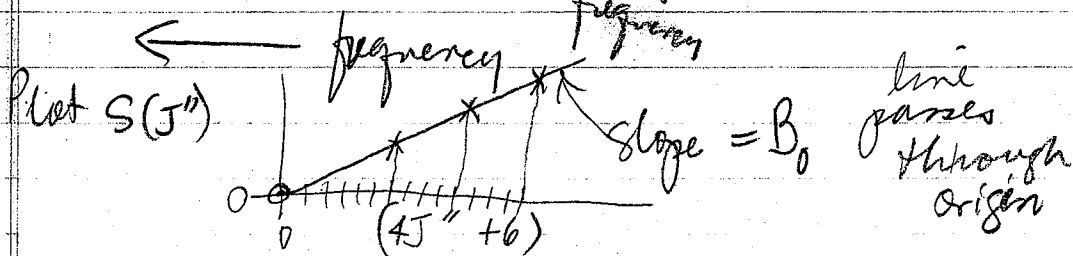
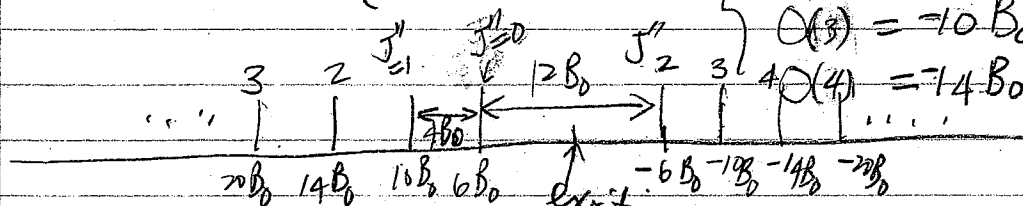
$$\begin{cases} S(0) = 6B_0 \\ S(1) = 10B_0 \\ S(2) = 14B_0 \end{cases}$$

$\Delta J = -2$ $J' = J'' - 2$ O branch begins with $J''=2$

$$O(J'') = B_0 \left[\underset{J^2 - 3J + 2}{(J''-2)(J''-1)} - \underset{J^2 - J}{J''(J''+1)} \right]$$

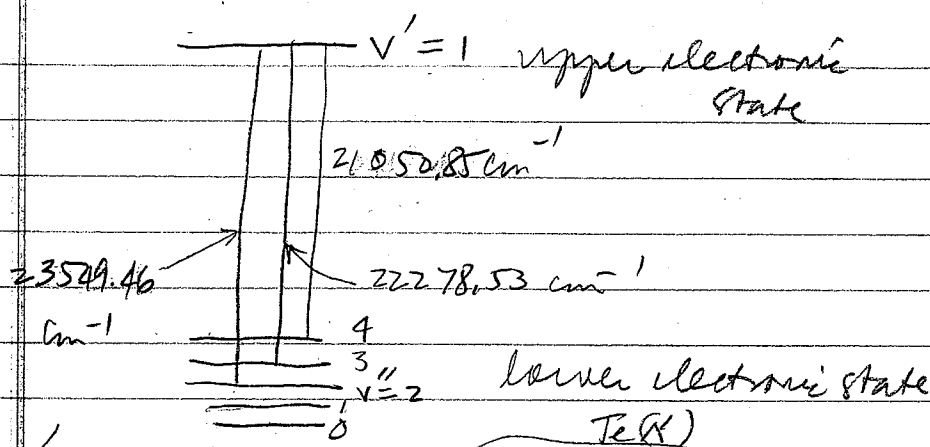
$$= -B_0(-4J'' + 2)$$

$$\begin{cases} O(2) = -6B_0 \\ O(3) = -10B_0 \\ O(4) = -14B_0 \end{cases}$$



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$$21050.85 = E_{v'=1} - E_{v''=0} = T_e(A') - T_e(A'') + \frac{3}{2}v_e' - \frac{9}{2}v_e'' - \left(\frac{3}{2}\right)^2 x_e v_e' + \left(\frac{9}{2}\right)^2 x_e v_e''$$

$$22278.53 = E_{v'=1} - E_{v''=3} = T_e(A') + \frac{3}{2}v_e' - \frac{3}{2}v_e'' - \left(\frac{3}{2}\right)^2 x_e v_e' + \left(\frac{7}{2}\right)^2 x_e v_e''$$

$$23549.46 = E_{v'=1} - E_{v''=2} = T_e(A') + \frac{3}{2}v_e' - \frac{5}{2}v_e'' - \left(\frac{3}{2}\right)^2 x_e v_e' + \left(\frac{5}{2}\right)^2 x_e v_e''$$

$$23549.46 - 22278.53 = -\frac{5}{2}v_e'' + \left(\frac{5}{2}\right)^2 x_e v_e'' + \frac{1}{2}v_e'' - \left(\frac{7}{2}\right)^2 x_e v_e''$$

$$= v_e'' - x_e v_e'' \left[\left(\frac{7}{2}\right)^2 - \left(\frac{5}{2}\right)^2 \right] = 1270.93$$

$$22278.53 - 21050.85 = -\frac{7}{2}v_e'' + \left(\frac{7}{2}\right)^2 x_e v_e'' + \frac{9}{2}v_e'' - \left(\frac{9}{2}\right)^2 x_e v_e''$$

$$= v_e'' - x_e v_e'' \left[\left(\frac{9}{2}\right)^2 - \left(\frac{7}{2}\right)^2 \right] = 1227.68$$

$$\text{next spacing} = -\frac{3}{2}v_e'' + \left(\frac{3}{2}\right)^2 x_e v_e'' + \frac{5}{2}v_e'' - \left(\frac{5}{2}\right)^2 x_e v_e'' = v_e'' - x_e v_e'' \left[\left(\frac{5}{2}\right)^2 - \left(\frac{3}{2}\right)^2 \right] =$$

$$\text{next spacing} = -\frac{1}{2}v_e'' + \left(\frac{1}{2}\right)^2 x_e v_e'' + \frac{3}{2}v_e'' - \left(\frac{3}{2}\right)^2 x_e v_e'' = v_e'' - x_e v_e'' \left[\left(\frac{3}{2}\right)^2 - \left(\frac{1}{2}\right)^2 \right]$$

(12)

If we sum over these spacings up to the $v''=4$ to $v'=1$, we get

$$4v_e'' - x_e v_e'' \left\{ \left(\frac{9}{2}\right)^2 - \left(\frac{7}{2}\right)^2 + \left(\frac{7}{2}\right)^2 - \left(\frac{5}{2}\right)^2 + \left(\frac{5}{2}\right)^2 - \left(\frac{3}{2}\right)^2 + \left(\frac{3}{2}\right)^2 - \left(\frac{1}{2}\right)^2 \right\}$$

$$= 4v_e'' - x_e v_e'' \left\{ \left(\frac{9}{2}\right)^2 - \left(\frac{1}{2}\right)^2 \right\}$$

This is the gap between $v''=0$ and $v''=4$ levels

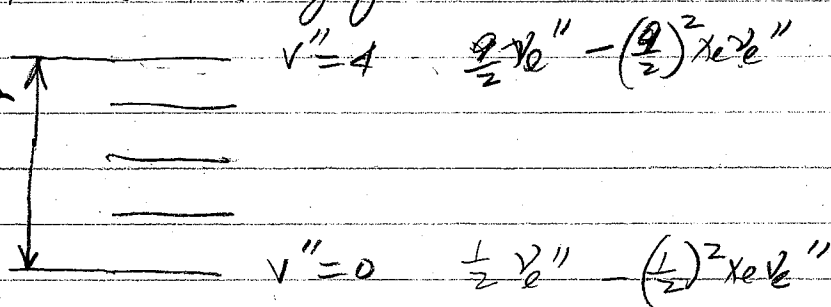
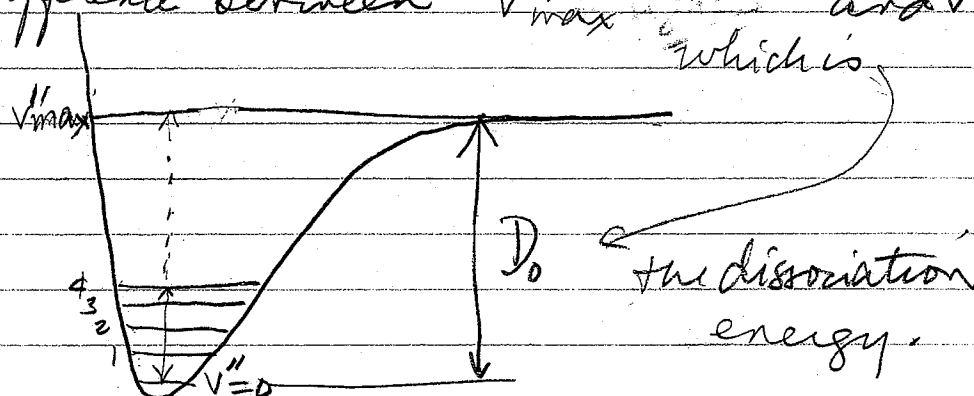


Diagram showing energy levels for $v''=0$ and $v''=4$. The gap is labeled as $\frac{9}{2}v_e'' - \left(\frac{9}{2}\right)^2 x_e v_e''$ for $v''=4$ and $\frac{1}{2}v_e'' - \left(\frac{1}{2}\right)^2 x_e v_e''$ for $v''=0$.

So if keep doing this sum through all the $v''=1$ to $v''=0$ through $v'=1$ to v''_{max} we should get all the way to the difference between v''_{max} and $v''=0$ which is



Part II

$J' = J'' + 2$ transitions

(13)

①

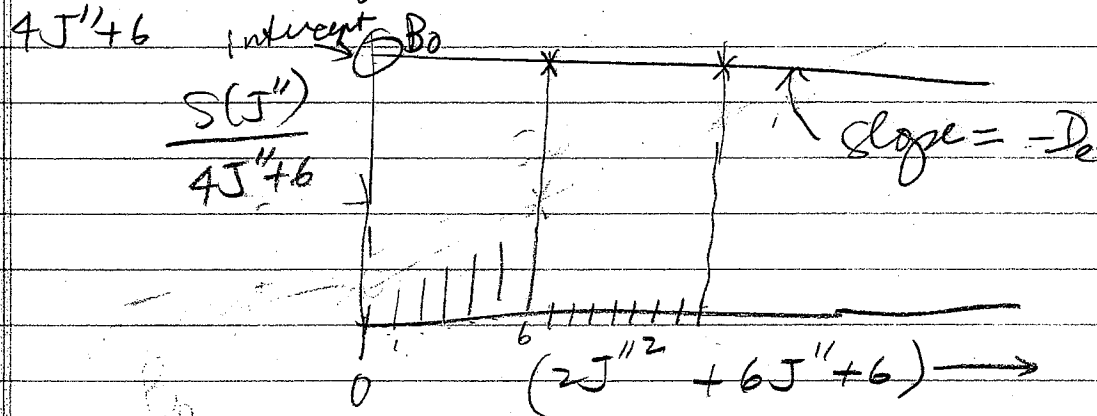
$$S(J'') = B_0 [(J''+2)(J''+3) - J''(J''+1)]$$

$$- D_e [(J''+2)^2 (J''+3)^2 - J''^2 (J''+1)^2]$$

$$= B_0 (4J''+6) - D_e (8J''^3 + 36J''^2 + 60J'' + 36)$$

$$S(J'') = B_0 (4J''+6) - D_e (4J''+6)(2J''+6J''+6)$$

$$\frac{S(J'')}{4J''+6} = B_0 - D_e (2J''^2 + 6J'' + 6)$$



answers: $B_0 =$

$D_e =$

Part II

(14)

② vibrational term is

$$G_v = \left(v + \frac{1}{2}\right) \nu_e - x_e \nu_e \left(v + \frac{1}{2}\right)^2$$

relative to $v=0$

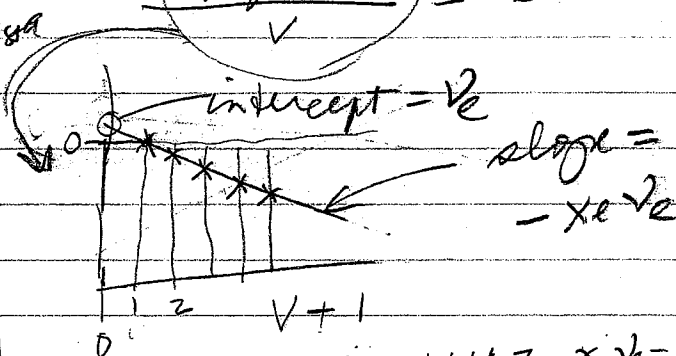
$$= \left(\frac{1}{2}\right) \nu_e + x_e \nu_e \left(\frac{1}{2}\right)^2$$

$$= v \cdot \nu_e - x_e \nu_e (v^2 + v)$$

given frequency

$$= \nu_e - x_e \nu_e (v+1)$$

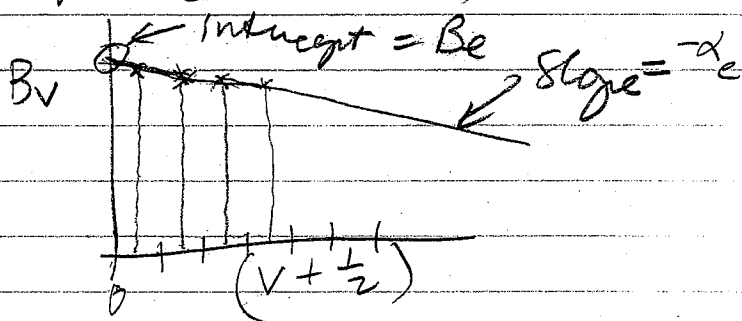
v	ordinate	abscissa
0	0	1
1	1406.51	2
2	2788.17	3
3	4139.71	4
4	5458.41	5
5	6745.52	6



answers: $\nu_e = 1444.71 \text{ cm}^{-1}$, $x_e \nu_e = 15.69 \text{ cm}^{-1}$

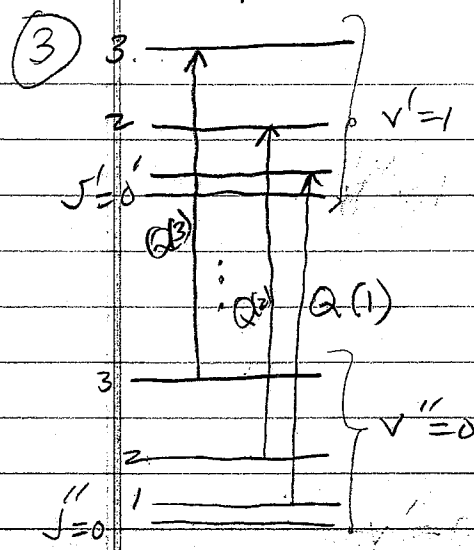
rotational constants are B_0, B_1, B_2 etc

$$B_v = B_e - \alpha_e \left(v + \frac{1}{2}\right)$$

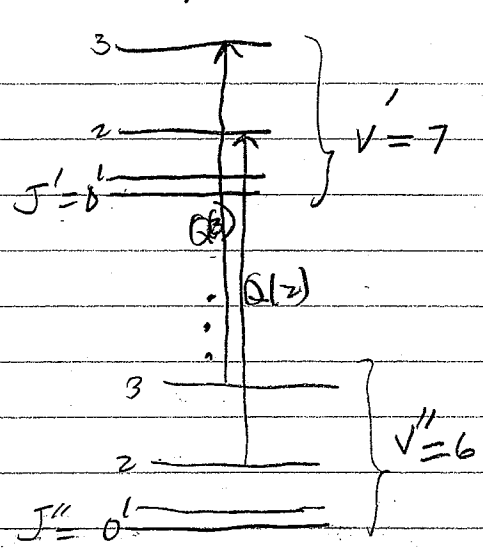


answers are: $B_e = 1.4667 \text{ cm}^{-1}$, $\alpha_e = 0.01992 \text{ cm}^{-1}$

ordinate	abscissa
1.4574	0.5
1.4366	1.5
1.4173	2.5
1.3937	3.5
1.3712	4.5
1.3561	5.5



$\Delta J = 0$ $^{15}\text{N}_2$



$\Delta J = 0$ $^{15}\text{N}_2$

spin of $^{15}\text{N} = \frac{1}{2}$

from hand-out on nuclear spin angular momentum

$Z = 7$ 7 protons 8 neutrons in ^{15}N

$$\left. \begin{array}{l} \text{protons } (1s_{1/2})^2 (1p_{3/2})^4 (1p_{1/2})^1 \\ \text{neutrons } (1s_{1/2})^2 (1p_{3/2})^4 (1p_{1/2})^1 \end{array} \right\} \text{net spin} = \frac{1}{2}$$

Pauli exclusion principle: Ψ_{TOTAL} must be antisymmetric with respect to interchange of ^{15}N nuclei in $^{15}\text{N}_2$ molecule

$$\Psi_{\text{TOTAL}} = \underbrace{\Psi_{\text{elec. space}}}_{\Lambda=0} \cdot \underbrace{\Psi_{\text{elec. spin}}}_{S, M_S} \cdot \underbrace{\Psi_{\text{vib.}}}_{v} \cdot \underbrace{\Psi_{\text{rot}}}_{J, M_J} \cdot \underbrace{\Psi_{\text{nuc. spin}}}_{I, M_I} \cdot F(X_{\text{cm}}) G(Y_{\text{cm}}) D(Z_{\text{cm}})$$

$P_{AB} \Psi_{\text{TOTAL}} = - \Psi_{\text{TOTAL}}$ if A and B are indistinguishable fermions (such as spin $\frac{1}{2}$ ^{15}N)

$$P_{AB} \Psi_{\text{elec. space}}^{\Lambda=0} = + \Psi_{\text{elec. space}}^{\Lambda=0} \text{ just like } \text{H}_2 \text{ molecule in Prob Set 12.}$$

where A and B enter into the electronic wavefunction since electron coordinates in atomic orbitals are on A+B

$P_{AB} \psi_{elec, spin} = + \psi_{elec, spin}$ since no A or B in $\psi_{elec, spin}$, it cannot change sign (16)

$P_{AB} \psi_{vib, v} = + \psi_{vib, v}$ since $(R_{AB} - R_e)$ does not change sign

$P_{AB} \psi_{rot, J, M_J} = P_{AB} Y_{J, M_J}(\theta, \phi) = (-1)^J Y_{J, M_J}(\theta, \phi)$ changes sign for odd J only

$P_{AB} \psi_{nuc, spin I, M_I} = P_{AB} \alpha(A) \cdot \alpha(B) = + \alpha(A) \cdot \alpha(B)$
 $P_{AB} \beta(A) \cdot \beta(B) = + \beta(A) \cdot \beta(B)$
 $P_{AB} [\alpha(A) \beta(B) + \beta(A) \alpha(B)] / \sqrt{2} = + () / \sqrt{2}$ } $I_{TOTAL} = 1$ three of these

$P_{AB} [\alpha(A) \beta(B) - \beta(A) \alpha(B)] / \sqrt{2} = - () / \sqrt{2}$ only one for $I_{TOTAL} = 0$

$P_{AB} (F \cdot G \cdot D)_{translation} = + (F \cdot G \cdot D)_{translation}$, since these

functions are entirely in center of mass coordinates

$$X_{CM} = \frac{m_A X_A + m_B X_B}{(m_A + m_B)}$$

interchanging A and B does not change the sign of X_{CM} and therefore cannot affect the sign of the function $\sqrt{\frac{2}{L_1}} \sin\left(\frac{n_x \pi}{L_1} X_{CM}\right)$

Thus the only parts that can change sign are rotation and nuclear spin. Must choose only those products of these functions that change sign

$$\begin{aligned} & Y_{odd, M}(\theta, \phi) \cdot \begin{cases} \alpha(A) \cdot \alpha(B) \\ \text{or } \beta(A) \cdot \beta(B) \\ \text{or } [\alpha(A) \beta(B) + \beta(A) \alpha(B)] / \sqrt{2} \end{cases} \\ & Y_{even, M}(\theta, \phi) \cdot [\alpha(A) \beta(B) - \beta(A) \alpha(B)] / \sqrt{2} \end{aligned}$$

We see that there are 3 ^{nuclear spin} states associated with odd J and only 1 nuclear spin state with even J . This fact alone would make $Q(\text{odd})$ three times as intense as the closest $Q(\text{even})$, if all states have equal likelihood.

For ^{14}N the nuclear spin is 1, resulting from
 7 protons $(\frac{1}{2})^2 (1 \frac{1}{2})^4 (1 \frac{1}{2})^1$ } total angular momentum
 7 neutrons $(\frac{1}{2})^2 (1 \frac{1}{2})^4 (1 \frac{1}{2})^1$ } of a ^{14}N nucleus
 is $\frac{1}{2} + \frac{1}{2} = 1$

Integer value of I makes ^{14}N a boson

Pauli exclusion principle states that I_{TOTAL} must be symmetric with respect to interchange of two indistinguishable bosons.

We already have seen that the only parts of the I_{TOTAL} of N_2 molecule that change sign upon P_{AB} are rotation and nuclear spin. From Prob-Set 12 you found the product functions that are eigenfunctions of I_{TOTAL}^2 and also M_I :

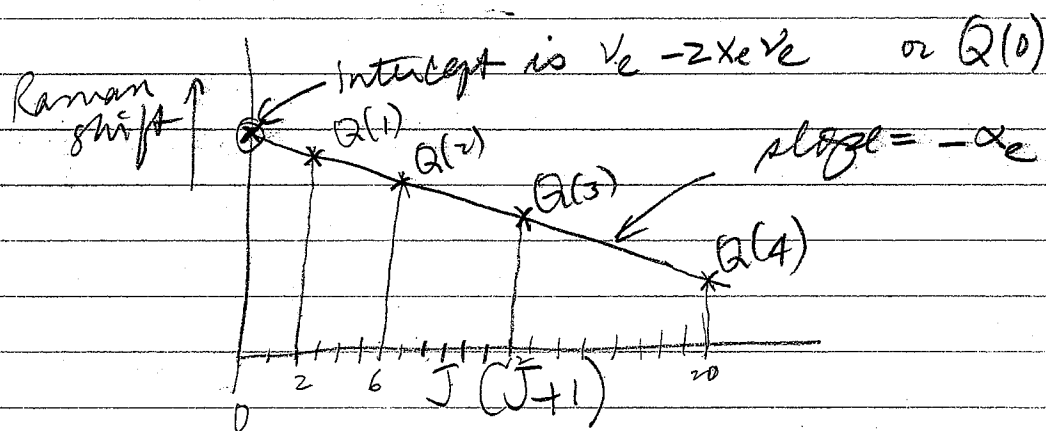
$$P_{AB} \left\{ \begin{array}{l} \alpha(A) \cdot \alpha(B) \\ \beta(A) \cdot \beta(B) \\ \gamma(A) \cdot \gamma(B) \\ [\alpha(A)\beta(B) + \beta(A)\alpha(B)]/\sqrt{2} \\ [\alpha(A)\gamma(B) + \gamma(A)\alpha(B)]/\sqrt{2} \\ [\beta(A)\gamma(B) + \gamma(A)\beta(B)]/\sqrt{2} \end{array} \right\} \quad \begin{array}{l} \text{no change in sign} \\ 6 \text{ functions for} \\ 6 \text{ states} \end{array}$$

$$P_{AB} \left\{ \begin{array}{l} [\alpha(A)\beta(B) - \beta(A)\alpha(B)]/\sqrt{2} \\ [\alpha(A)\gamma(B) - \gamma(A)\alpha(B)]/\sqrt{2} \\ [\beta(A)\gamma(B) - \gamma(A)\beta(B)]/\sqrt{2} \end{array} \right\} \rightarrow \begin{array}{l} \text{change in sign} \\ 3 \text{ functions for} \\ 3 \text{ nuclear spin states} \end{array}$$

(19)

$Q(J)$
frequency of Raman shift is given by:

$$\begin{aligned}
 E_{v=1,J} - E_{v=0,J} &= \left(\frac{3}{2} \nu_e\right) - x_e \nu_e \left(\frac{3}{2}\right)^2 \\
 &\quad - \alpha_e \left(\frac{3}{2}\right) J(J+1) \\
 &\quad - \left[\frac{1}{2} \nu_e - x_e \nu_e \left(\frac{1}{2}\right)^2 - \alpha_e \left(\frac{1}{2}\right) J(J+1) \right] \\
 &= \nu_e - 2x_e \nu_e - \alpha_e J(J+1)
 \end{aligned}$$



largest Raman shift is $Q(0)$, decreasing with increasing J

Part II continued

(20)

④ We see from number ⑤ of Part I that

$$1270.87 = T_e(\Lambda') + \frac{3}{2}v_e' - \left(2 + \frac{1}{2}\right)v_e'' - \left(2 + \frac{1}{2}\right)^2 x_e v_e''$$

$$- \left[T_e(\Lambda') + \frac{3}{2}v_e' - \left(3 + \frac{1}{2}\right)v_e'' - \left(3 + \frac{1}{2}\right)^2 x_e v_e'' \right]$$

$$= -G_{v'' + \frac{1}{2}}(v'' = 2) + G_{v'' + \frac{1}{2}}(v'' = 3)$$

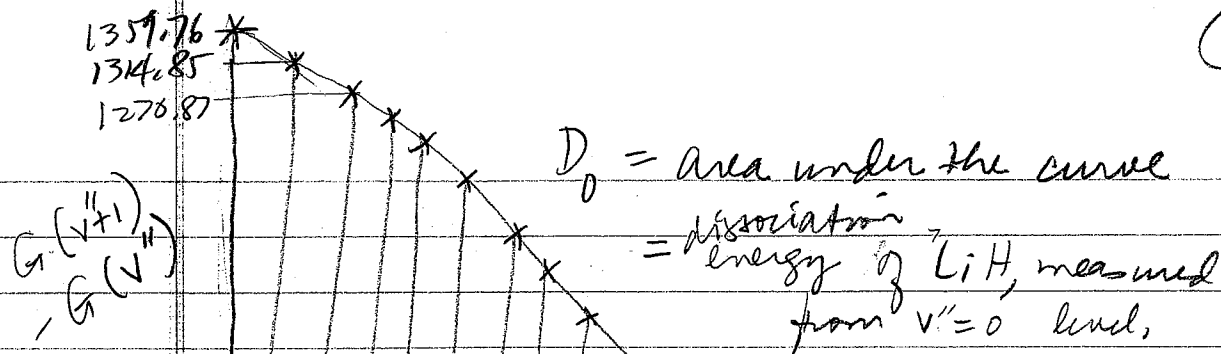
for Λ'' state, the lower electronic state
Therefore we identify all the other frequencies as

From the given table

assignment

cm^{-1}	$v'' + \frac{1}{2}$	
1359.76	$0 + \frac{1}{2}$	$G_{v'' + \frac{1}{2}}(v'' = 1) - G_{v'' + \frac{1}{2}}(v'' = 0)$
1314.85	$1 + \frac{1}{2}$	$G_{v'' + \frac{1}{2}}(v'' = 2) - G_{v'' + \frac{1}{2}}(v'' = 1)$
1276.87	$2 + \frac{1}{2}$	$G_{v'' + \frac{1}{2}}(v'' = 3) - G_{v'' + \frac{1}{2}}(v'' = 2)$
1227.82	$3 + \frac{1}{2}$	
1185.40	$4 + \frac{1}{2}$	
1143.83	$5 + \frac{1}{2}$	
1102.63	$6 + \frac{1}{2}$	
1061.74	$7 + \frac{1}{2}$	
1021.16	$8 + \frac{1}{2}$	
980.42	$9 + \frac{1}{2}$	
939.97	$10 + \frac{1}{2}$	
897.97	$11 + \frac{1}{2}$	$G_{v'' + \frac{1}{2}}(v'' = 12) - G_{v'' + \frac{1}{2}}(v'' = 11)$

(2)



$$\sum_{v''=0}^{v''_{\max}} [G(v''+1) - G(v'')] \cong \text{area under the straight line}$$

$$= \frac{1}{2} (32) (1359.76)$$

$$= 21756.16 \text{ cm}^{-1}$$

